

TSD 03

Determination of characteristic compressive strength of masonry, fk

Currently in the UK, masonry design may be carried out in accordance with Eurocode 6 (EC6) EN1996-1-1 or the withdrawn British Standard BS5628 (withdrawn meaning that it will no longer be maintained or updated by BSI). A basic difference between the EC6 approach and that of BS5628 is that EC6 uses a formula to calculate the characteristic compressive strength of masonry, f_k , whereas BS5628:Pt1 is based on tabulated values.

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These tables take into account mortar mixes, different sizes of units (height to thickness ratios) and strength of units. Although previously unit strengths in the UK were based on saturated units (in accordance with BS6073), these have now been replaced by air dry strength values in accordance with the European product standards (EN 771 series) - block strengths in BS5628 were changed to reflect this so that, for example, an old 7.0N/mm² is now 7.3N/mm². For designs to BS5628, the characteristic compressive strength of masonry, f_k , should be obtained from Tables 2a - 2h (based on mortar strength and size of masonry unit). Given below are values interpolated from BS5628 Table 2 which are relevant to walls constructed with H+H aircrete blocks.

				Designation (iii) / M4 mortar					elfix thin l	ayer mor	tar
				(declared	Block type compressive	strength)		Block type (declared compressive strength)			
					High	Super	Aggregate			High	Super
Blo Height	ock Thickness	H/t	Solar (2.9)	Standard (3.6)	Strength (7.3)	Strength (8.7)	block* (10.4)	Solar (2.9)	Standard (3.6)	Strength (7.3)	Strength (8.7)
	215	0.65	1.5	1.8	3.3	3.7		1.5	1.8	3.5	4.0
140	300	0.47	1.3	1.5	2.9	3.3		1.3	1.5	3.1	3.5
	350	0.40	1.2	1.4	2.7	3.1		1.2	1.4	2.9	3.3
	75	2.87	2.8	3.5	6.4	7.2		2.8	3.5	6.8	7.7
	100	2.15	2.8	3.5	6.4	7.2	8.2	2.8	3.5	6.8	7.7
	140	1.54	2.3	2.9	5.3	6.0	6.8	2.3	2.9	5.7	6.4
	150	1.43	2.2	2.8	5.1	5.8	6.5	2.2	2.8	5.4	6.1
215	200	1.08	1.9	2.3	4.3	4.8		1.9	2.3	4.6	5.2
210	215	1.00	1.8	2.2	4.1	4.6	5.3	1.8	2.2	4.4	4.9
	275	0.78	1.6	1.9	3.6	4.1		1.6	1.9	3.8	4.3
	300	0.72	1.5	1.8	3.5	3.9		1.5	1.8	3.7	4.2
	325	0.66	1.5	1.8	3.3	3.8		1.5	1.8	3.5	4.0
	350	0.61	1.4	1.7	3.2	3.6		1.4	1.7	3.4	3.9
250	100	2.50						2.8	3.5	6.8	7.7
200	140	1.79						2.6	3.2	6.3	7.1
350	100	3.50						2.8	3.5	6.8	7.7

Table 1: Characteristic compressive strength, fk, of masonry (to BS5628:Pt1) for H+H aircrete blocks

* Aggregate block by others, included for comparison purposes only

All thicknesses shown in each strength for comparison purposes. Please consult H+H Sales Office 01732 886444 for availability of sizes.

Given the vast array of different materials, sizes and shapes of units available across Europe, it was decided when developing EC6 that a single formula approach would be more viable than a tabulated one. However, in order for this to work then the compressive strength of each unit would have to be standardised or "normalised". The normalised mean compressive strength, f_b , used in EC6 is the compressive strength of an air dry 100mm cube of a masonry unit.

Normalised compressive strength, f_b, of blocks

The normalised compressive strength of a masonry unit is a calculated value used to determine the wall strength and should not be confused with the declared mean compressive strength of a block which is a measured property. The values currently declared by manufacturers in the UK are mean air dry strengths for the complete brick or block unit (eg for aircrete 2.9, 3.6, 7.3 and 8.7N/mm²). Compressive strengths are given in N/mm², ie it is the compressive stress of material. The thickness of the blocks are therefore irrelevant (although a 140mm thick block will obviously carry more load than a 100mm block by virtue of its greater area). In order to obtain the normalised strength, the declared mean strengths will need to be multiplied by a shape factor relative to the size of the unit.



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The value of the shape factor is given in Table A.1 of EN 772-1 (relevant values applicable to H+H blocks have been interpolated and are given in the table below).

Although it appears that compressive strength varies with size, it is worth noting that it is not the strength of the masonry unit which alters with its size but merely the effect it has on the overall strength of the wall into which is built.

Table 2: Normalised compressive strengths, f_b, for H+H aircrete blocks in N/mm²

			Block type							
				(declared compressive strength, N/mm ²)						
					High	Super	Aggregate			
Block			Solar	Standard	Strength	Strength	block*			
Height	Thickness	Shape factor	(2.9)	(3.6)	(7.3)	(8.7)	(10.4)			
140	215	0.95	2.7	3.4	6.9	8.2				
140	250 +	0.91	2.6	3.3	6.6	7.9				
	75	1.43	4.1	5.1	10.4	12.4				
	100	1.38	4.0	5.0	10.1	12.0	14.4			
	140	1.30	3.8	4.7	9.5	11.3	13.5			
215	150	1.28	3.7	4.6	9.3	11.1	13.3			
	200	1.18	3.4	4.2	8.6	10.3				
	215	1.16	3.4	4.2	8.5	10.1	12.1			
	250 +	1.12	3.2	4.0	8.1	9.7				
250	100	1.45	4.2	5.2	10.6	12.6				
200	140	1.37	4.0	4.9	10.0	11.9				
350	100	1.45	4.2	5.2	10.6	12.6				

* Aggregate block by others, included for comparison purposes only

The characteristic compressive strength of masonry designed to BS EN 1996-1 is given by

$$f_k = K \cdot f_b^{\alpha} \cdot f_m^{\beta}$$

Clause 3.6.1.2(1)(i)

Where f_b is the normalised compressive strength of the unit, f_m is the mortar strength (not greater than f_b) and K, α and β are constants taken from the UK National Annex.

	Designation (iii) / M4 mortar						Celfix thin layer mortar				
$(K = 0.75, \alpha = 0.7, \beta = 0.3, fm = 4N/mm^2)$					$(K = 0.9, \alpha = 0.85, \beta = 0, fm = 10N/mm^2)$						
				Block type			Block type				
			(declared cor	mpressive stre	· · · ·		(decla	ared compress	U 1	,	
				High	Super	Aggregate			High	Super	
Blo	ock	Solar	Standard	Strength	Strength	block*	Solar	Standard	Strength	Strength	
Height	Thickness	(2.9)	(3.6)	(7.3)	(8.7)	(10.4)	(2.9)	(3.6)	(7.3)	(8.7)	
140	215	2.1	2.6	4.4	5.0		2.1	2.5	4.6	5.4	
140	250 +	2.0	2.5	4.3	4.8		2.1	2.5	4.5	5.2	
	75	2.9	3.6	5.9	6.6		2.9	3.6	6.6	7.7	
	100	2.9	3.5	5.7	6.5	7.3	2.9	3.5	6.4	7.4	
	140	2.8	3.3	5.5	6.2	7.0	2.8	3.3	6.1	7.1	
215	150	2.8	3.3	5.4	6.1	7.0	2.7	3.3	6.0	7.0	
	200	2.6	3.1	5.1	5.8		2.6	3.1	5.6	6.5	
	215	2.5	3.1	5.1	5.7	6.5	2.5	3.0	5.5	6.4	
	250 +	2.4	3.0	4.9	5.6		2.4	2.9	5.3	6.2	
250	100						2.9	3.6	6.7	7.8	
250	140						2.9	3.5	6.4	7.4	
350	100						2.9	3.6	6.7	7.8	

* Aggregate block by others, included for comparison purposes only

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Determination of vertical load resistance of a wall

It should be noted that it would not be correct to compare fk values in isolation as the determination of characteristic compressive strength of the masonry is a starting point for determining the load bearing capacity of a wall rather than a final answer. The load resistance of a wall depends not only on its compressive strength but also on its height, length, restraint conditions etc.

For example, the design vertical load resistance of a wall is given in BS5628 as $(\beta.t.f_k)/\gamma_m$ where β is the capacity reduction factor allowing for the effect of slenderness and load eccentricity. Similarly, in EC6 it is given by \emptyset .t.(f_k/γ_M). where Ø is the capacity reduction factor allowing for the effect of slenderness and load eccentricity.

However, the similarity ends there because there are significant differences in the way the two codes calculate slenderness and eccentricities. Consequently, although the comparative f_k values appear different to start with, the final answers in terms of the load resistance of a wall should be fairly similar. It is worth noting, therefore, that specific values obtained whilst working with the two codes are not interchangeable (eg fk obtained using one code should not be applied to the other).

National Annex

As with the product standards, standardising design codes across Europe has proved to be a complicated and long drawn out process. Whilst the aim was to adopt a single design procedure, it was also equally, if not more, important not to end up with a document which would give significantly different answers to those obtained using existing National Standards in each country - hence the introduction of the National Annexes.

It is therefore important to work with the National Annex to EN1996-1 as the figures given therein have been specifically developed to give a final answers which are comparable to design calculations made to BS5628. The latest version of BS EN1996-1-1 was published in early 2013 along with a revised UK National Annex.

Characteristic flexural strength of masonry, f_{kx}

The design for lateral load in EC 6 is based on UK design practice and is similar to BS5628:Pt 1 with the values for characteristic flexural strength in the National Annex being identical to the values BS5628. Interpolated figures relevant to H+H aircrete are given in Table 4 below.

Ŧ.	4. Characteristic nexulai strength, Γ_{xk1} and Γ_{xk2} , of masoning to EC 0 for Π Π and refere blocks in which										
		Values of	f _{kx1}			Values of f _{kx2}					
		Plane of fai	lure parallel to	bed joints		Plane of failure perpendicular to bebjoints					
_											
			Block	type			Block	type			
	Block	(decla	ared compress	ive strength, N	'mm²)	(decla	ared compress	ive strength, N	'mm²)		
	thickness			High	Super			High	Super		
		Solar	Standard	Strength	Strength	Solar	Standard	Strength	Strength		
	(mm)	(2.9)	(3.6)	(7.3)	(8.7)	(2.9)	(3.6)	(7.3)	(8.7)		
	75		0.	25		0.40	0.45	0.60	0.60		
	100		0.1	25		0.40	0.45	0.60	0.60		
	140		0.	22		0.36	0.40	0.53	0.53		
	150		0.:	22		0.35	0.38	0.52	0.52		
	200		0.	18		0.30	0.32	0.43	0.43		
	215		0.	17		0.29	0.30	0.41	0.41		
	250 +		0.	15		0.25	0.25	0.35	0.35		

Table 4: Characteristic flexural strength, fund and fundation of masonry to EC 6 for H+H aircrete blocks in N/mm²

Values applicable to walls built with both traditional M4 mortar or H+H Celfix thin layer mortar



Benefits of Celfix thin layer mortar

Effect of thin layer mortar on characteristic compressive strength

Although BS5628 recognises the use of thin layer mortars, the benefit in design is limited as the code states that the characteristic wall compressive strengths tabulated for Designation (i), or M12, mortars should be used. Wider European experience of thin layer mortars has meant that the formula derived for EC6 gives more enhanced values for walls built using thin layer mortars when compared to traditional mortars.

Fig 1 below shows the characteristic compressive strength, f_k , to EC6 for a wall built using our Celfix thin layer mortar and a traditional designation (iii) M4 mortar, both with our High Strength (7.3N/mm²) blocks. For a 100mm thick wall, an enhancement of 12% can be achieved by adopting a thin layer mortar in conjunction with High Strength. Similarly, an enhancement of up to 15% can be achieved for Super Strength blockwork. These can be further improved if used in combination with our larger format (250mm high) Jumbo blocks.

The improvement effect of thin layer mortar is less pronounced with Standard grade blocks (3 - 4%) and negligible with Solar due to the fact that the mortar strength is limited to block strengths in the formulae for f_k .

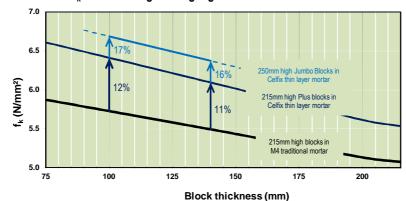


Fig 1: Comparison of EC6 fk values for High Strength grades of H+H blockwork

Effect of partial safety factors

Both compressive and flexural design strengths incorporate a material partial safety factor in their determination. H+H High Strength (7.3N/mm²) and Super Strength (8.7N/mm²) blocks are manufactured to special category of manufacturing control (ie Category I) which permits a reduced material partial safety factor to be used in design calculations. Furthermore, our Celfix thin layer mortar is factory produced to BS EN 998-2 which enables the utilisation of special category of construction control (Class 1 execution control in EC6).

These two factors combined mean that a reduced partial safety factor, γ_m , of 2.5 (BS 5628:Pt1 Table 4) may be used for both compression and flexure when designing to BS 5628 (see Table 5 below).

This can be equivalent to an additional improvement of at least 20% to wall strength when compared to the safety factors of 3.1 or 3.5 normally assumed.

Standard (3.6N/mm²) and Solar (2.9N/mm²) blocks are normal category (Category II), therefore a slightly higher safety factor of 2.8 applies to compressive strength although 2.5 is still applicable for flexure.

Table 5: Partial Safety	γ factors for material strength $\gamma_{ m r}$	from BS5628:Pt 1 Table 4

	Grade of H+H	aircrete	Category of manufacturing control		egory of con al mortar Normal	struction control H+H Celfix thin layer mortar *
Compression, γ_m	Super Strength High Strength	(8.7N.mm²) (7.3N.mm²)	Category I	2.5	3.1	2.5
	Standard Solar	(3.6N.mm ²) (2.9N.mm ²)	Category II	2.8	3.5	2.8
Element of	Super Strength High Strength	(8.7N.mm²) (7.3N.mm²)	Category I	0.5	2.0	0.5
Flexure, $\gamma_{\sf m}$	Standard Solar	(3.6N.mm²) (2.9N.mm²)	Category II	2.5	3.0	2.5

* Use of H+H Celfix thin layer mortar would enable Special category of construction control to be assumed



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For designs to EC6, the UK National Annex offers similar, though less pronounced, benefits. Values for γ_M for the ultimate limit state are given in Table NA.1 of the National Annex (see Table 6 below).

In addition, it offers advantages to designers with regards to safety factors where the masonry is an infill panel to a framed structure. Panels within a framed structure can be classified as being in 'laterally loaded wall panel when the removal of the panel would not affect the overall stability of the building'.

Table 6: Partial Safety factors	for material strength YM from NA	. to BS EN 1996-1-1, Ta	ble NA.1

Grade of H+H aircrete		Category of manufacturing control	Class of exec Traditional mortar 1 2		cution control H+H Celfix thin layer mortar *	
	Super Strength High Strength	(8.7N.mm²) (7.3N.mm²)	Category I	2.3	2.7	2.3
Compression, γ_{M}	Standard Solar	(3.6N.mm²) (2.9N.mm²)	Category II	2.6	3.0	2.6
Flexure, γ_{M}	Super Strength High Strength	(8.7N.mm²) (7.3N.mm²)	Category I	2.3	2.7	2.3
(when removal of panel would affect overall stability of the building)	Standard Solar	(3.6N.mm²) (2.9N.mm²)	Category II	2.5		2.0
Flexure, γ_{M}	Super Strength High Strength	(8.7N.mm²) (7.3N.mm²)	Category I	2.0	2.4	2.0
(when removal of panel would not affect overall stability of the building)	Standard Solar	(3.6N.mm²) (2.9N.mm²)	Category II	2.0	2.4	2.0

* Use of H+H Celfix thin layer mortar would enable Class 1 execution control to be assumed

Further information regarding design to EC6 may be obtained via a website dedicated to Eurocode 6 (www.eurocode6.org) or by contacting our Technical Services Department.